



# Fast neutron irradiation facilities in MARIA reactor

*fission neutrons for fusion materials*

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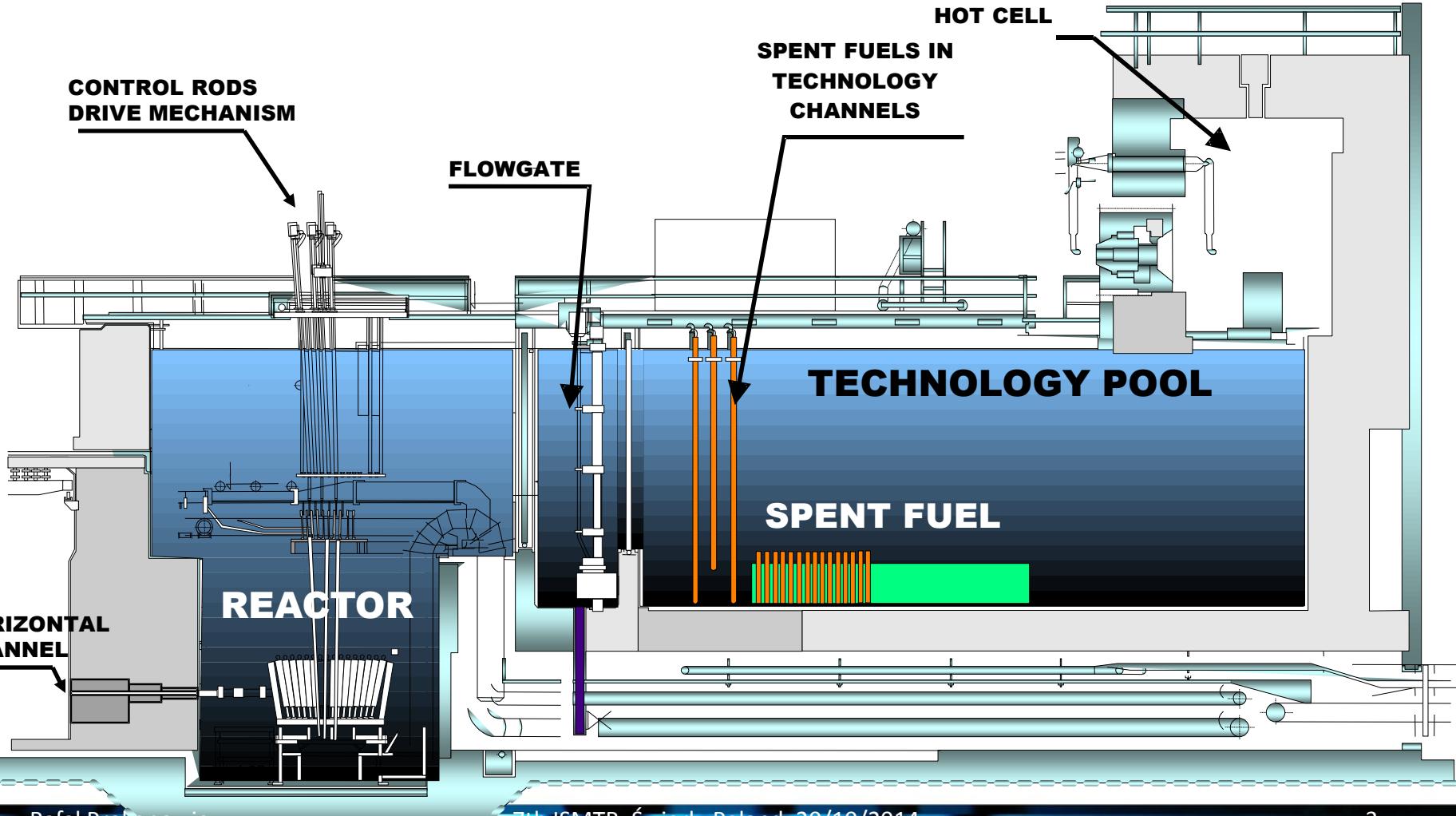
National Centre for Nuclear Research  
Świerk, Poland

7<sup>th</sup> International Symposium on Material Testing Reactors

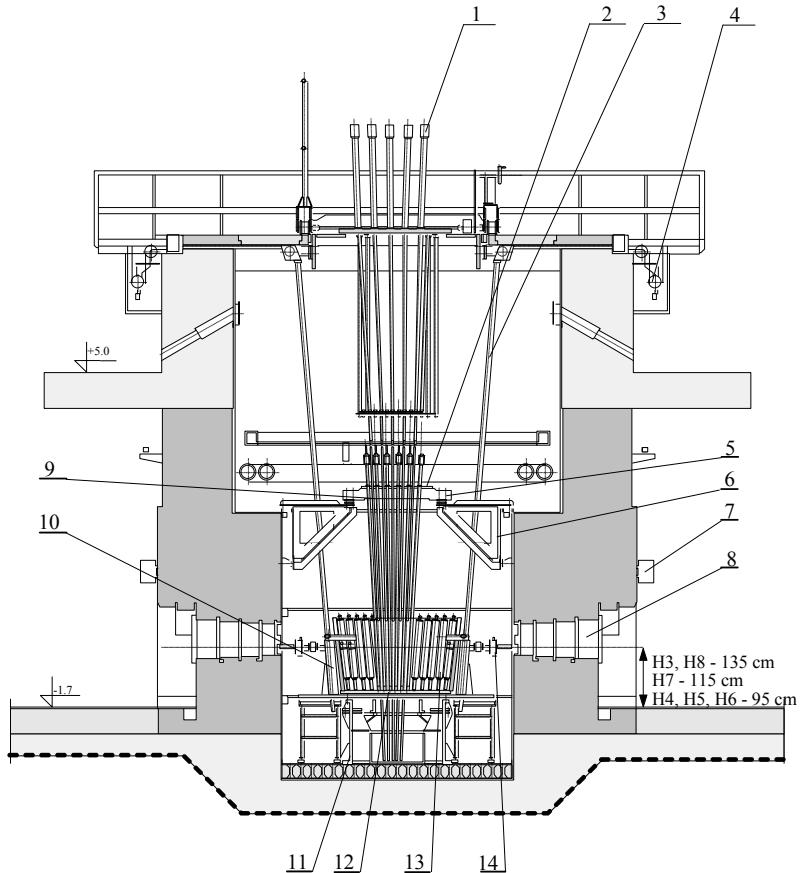
# MARIA Research Reactor

- high neutron flux density research reactor
- water and beryllium moderated
- pool-type reactor with pressurized fuel channels
- concentric tube assemblies of fuel elements
- fuel channels in conical matrix of beryllium blocks surrounded by graphite reflector
- 30 MW of nominal thermal power
- thermal neutron flux density up to  $2 \cdot 10^{14} \text{ cm}^{-2} \text{ s}^{-1}$
- fast neutron flux density up to  $3 \cdot 10^{13} \text{ cm}^{-2} \text{ s}^{-1}$
- over 4000 hours operation per year
- radioisotope production 600 TBq/year
- Mo-99 production 6000 TBq/year

# MARIA reactor

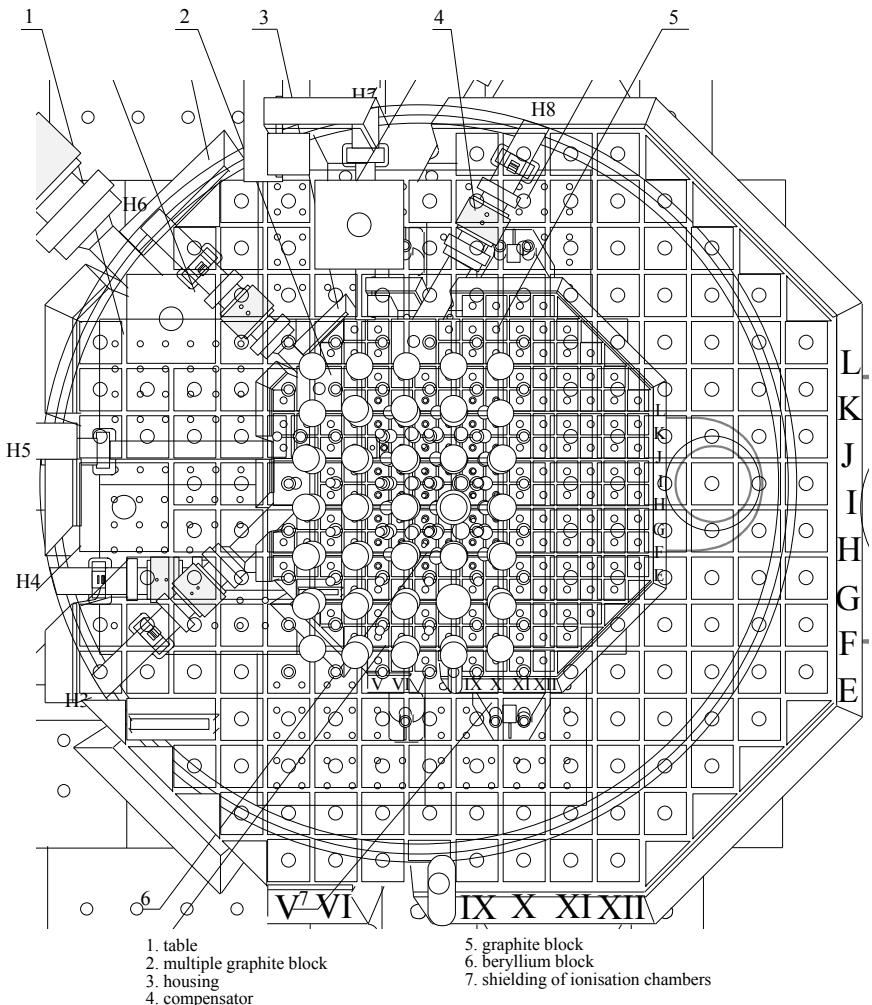


# MARIA reactor

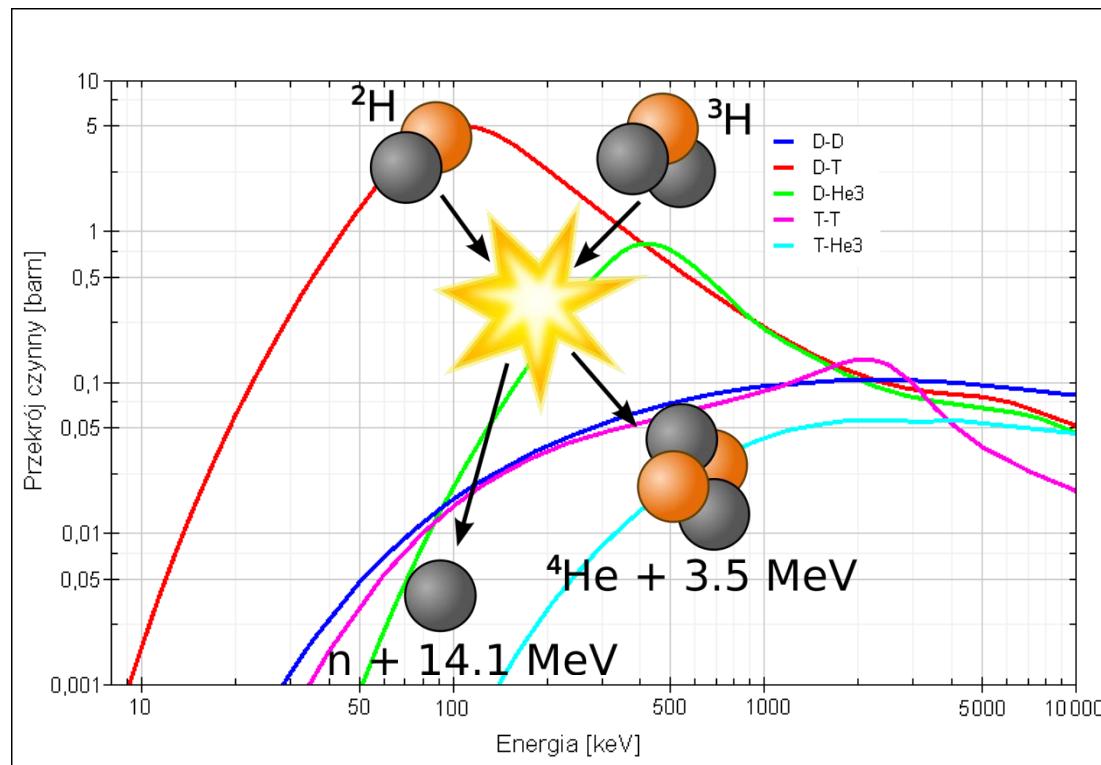


- 1. control rod drive
- 2. mounting slab
- 3. ionisation chamber channel
- 4. ionisation chamber drive
- 5. slab supporting structure
- 6. slab bracket
- 7. horizontal beam slide damped drive

- 8. horizontal beam slide damper
- 9. fuel channel
- 10. ionization chamber shielding
- 11. basket basis
- 12. reflector housing
- 13. reflector blocks
- 14. horizontal neutron beam compensator

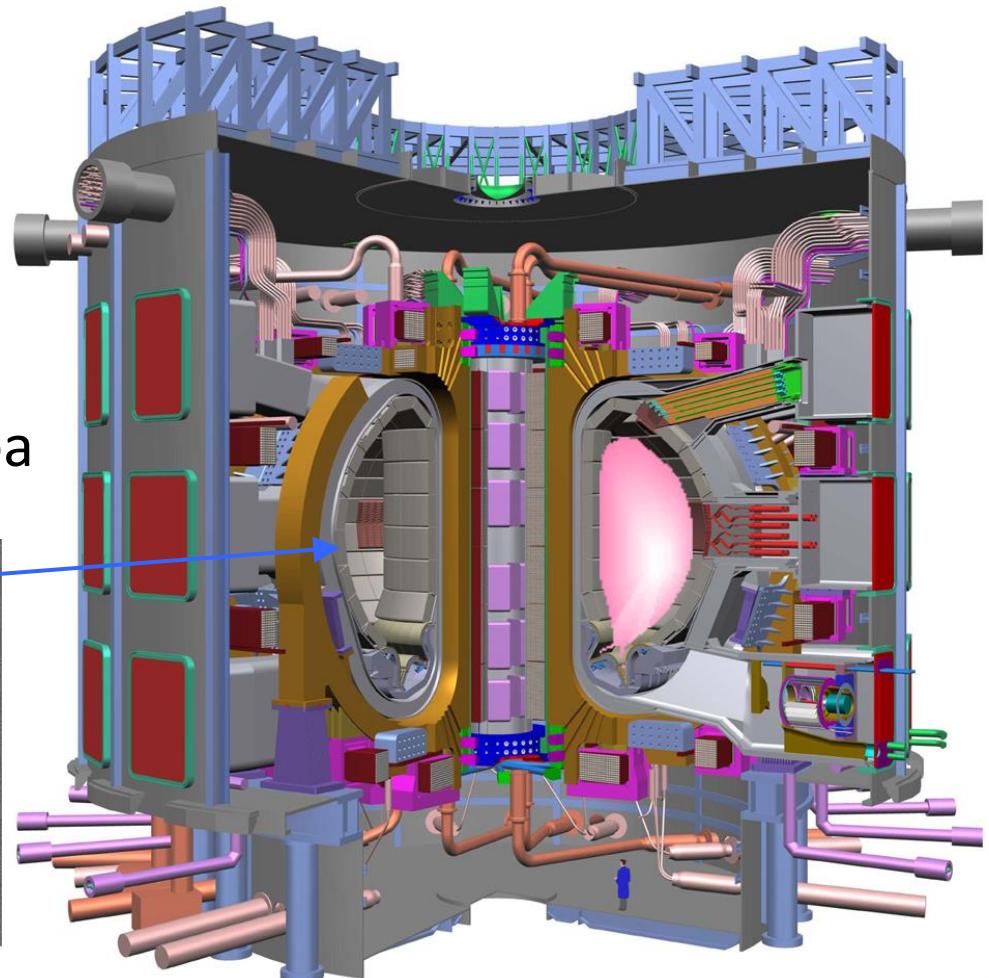
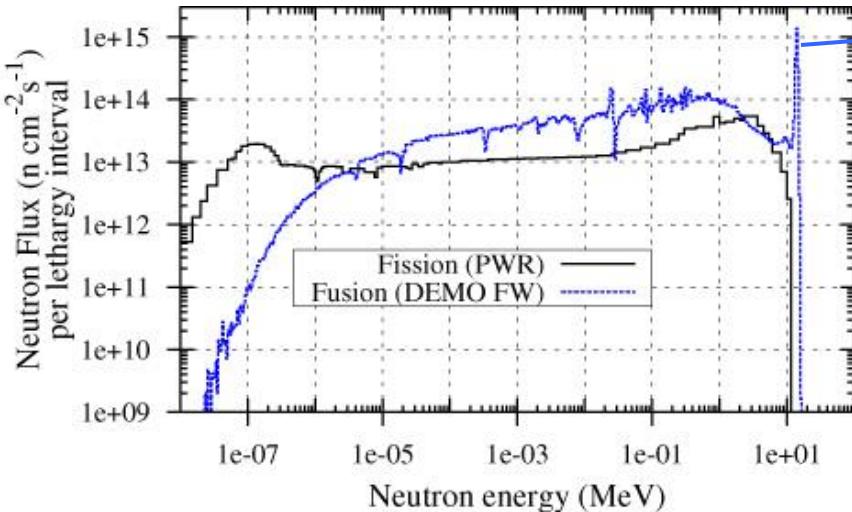


# Neutrons from fusion



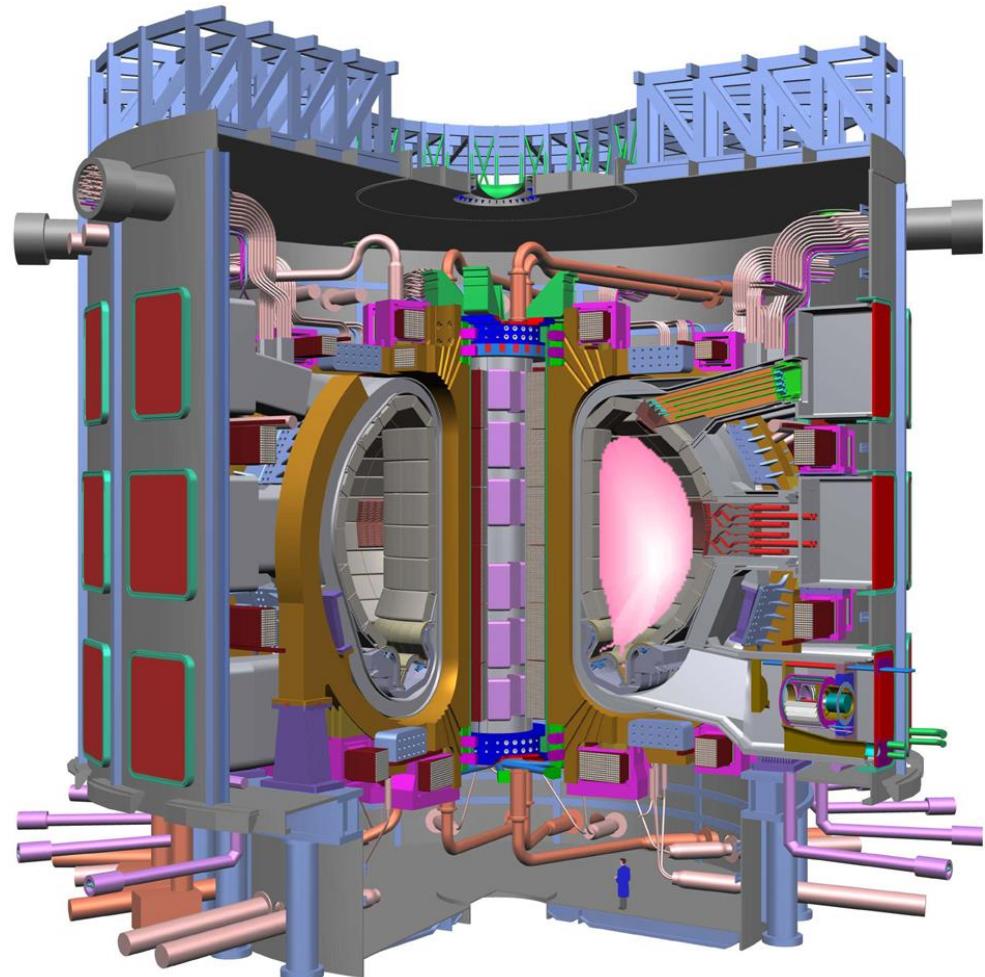
# Fusion reactor

- heat load  $10 \text{ MW/m}^2$
- temperature  $4\text{K}\div800\text{K}$
- fast neutron flux density  
 $3 \cdot 10^{14} \text{ cm}^{-2} \text{ s}^{-1}$
- structure degrad.  $3\div150 \text{ dpa}$



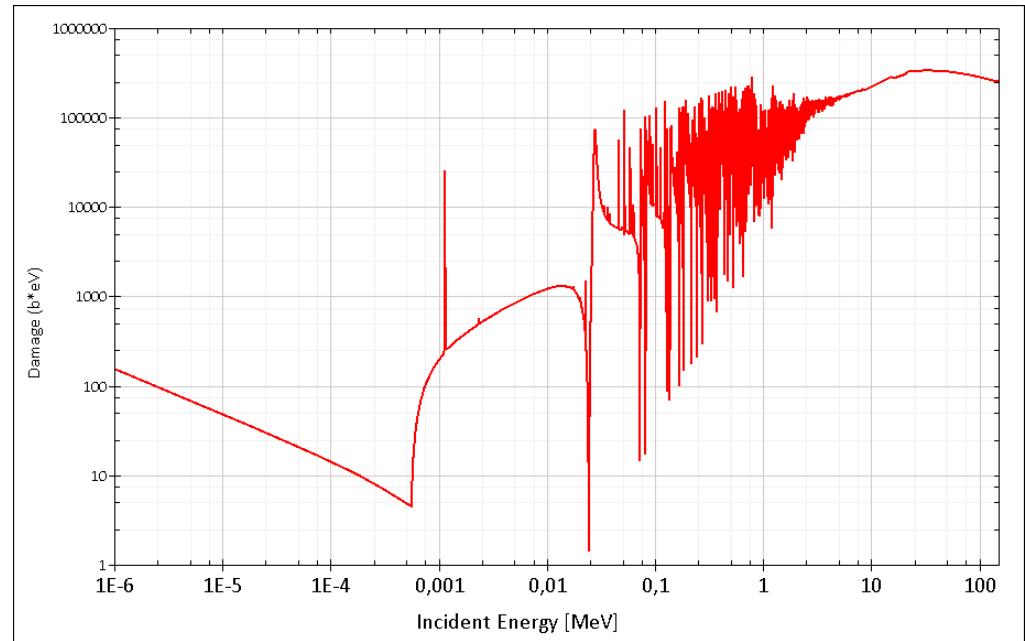
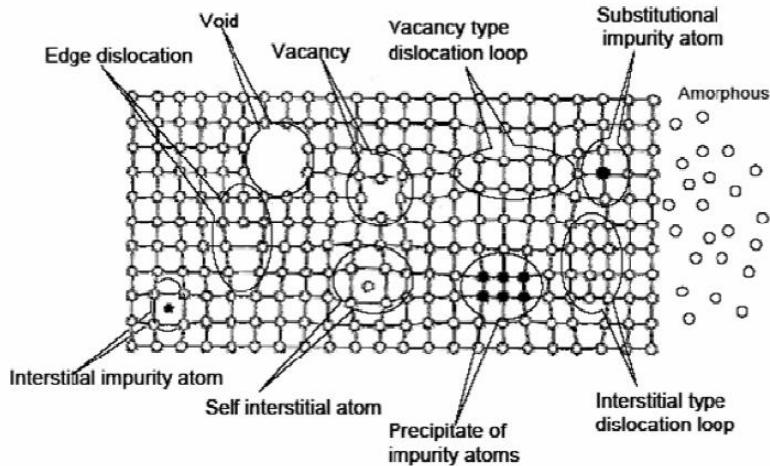
## Fusion materials

- beryllium (1st wall, blanket)
- lithium compounds
- tungsten (divertor)
- carbon fibre composite (divertor)
- austentic steel
- nickel alloys
- titanium alloys
- ferritic steel
- ceramics (insulators)



# Structure degradation

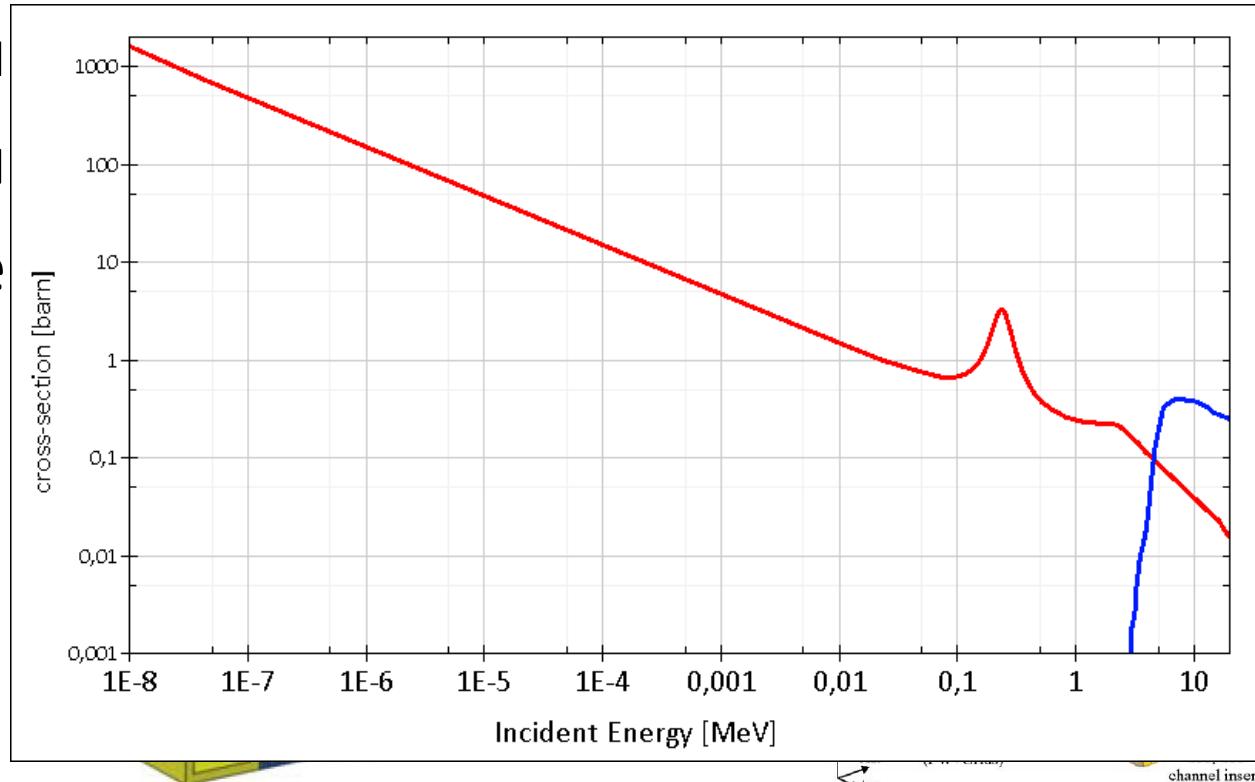
displacement per atom (dpa)



# Tritium breeding

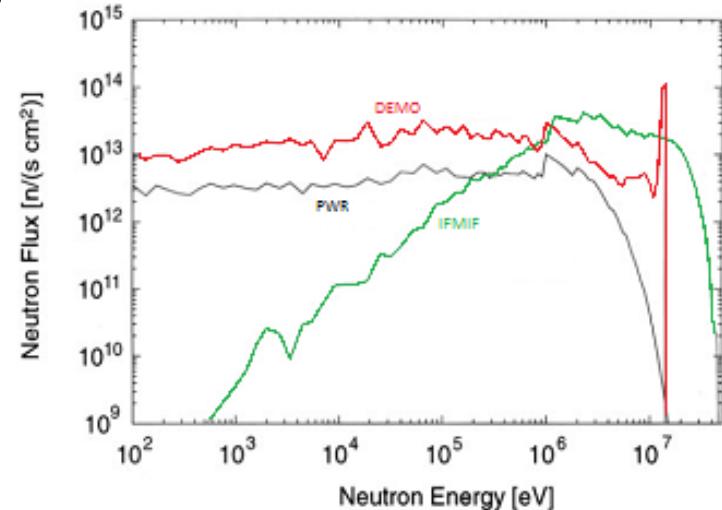
Breeding  ${}^6\text{Li} + \text{n} \rightarrow \text{T} + {}^4\text{He}$        ${}^7\text{Li} + \text{n} \rightarrow \text{T} + {}^4\text{He} + \text{n}$

- helium
- helium
- water

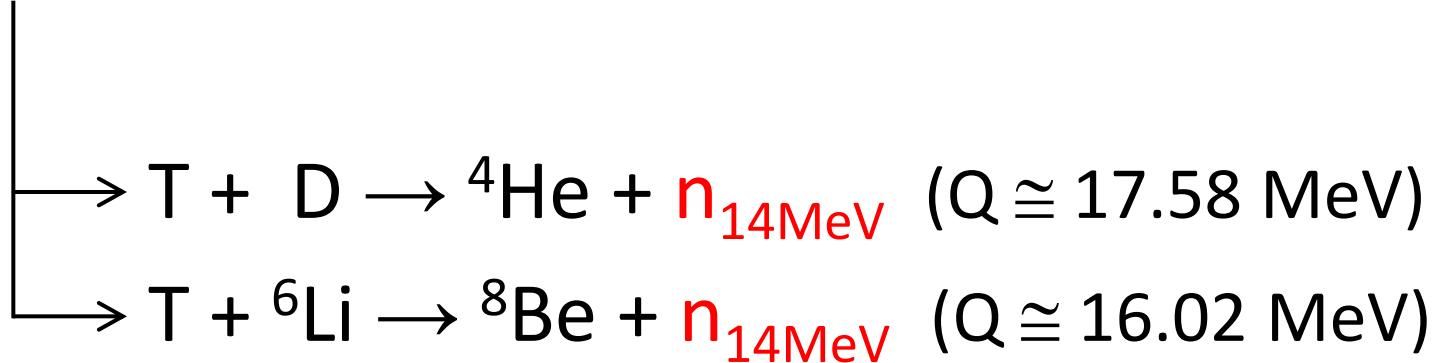


# The 14 MeV neutron sources

- accelerator sources
  - solid target (ASP AWE  $\sim 2 \cdot 10^{10} \text{ cm}^{-2} \text{ s}^{-1}$ , FNG  $\sim 1 \cdot 10^9 \text{ cm}^{-2} \text{ s}^{-1}$ , IFJ  $\sim 1 \cdot 10^7 \text{ cm}^{-2} \text{ s}^{-1}$ )
  - plasma target (GDT, Nowosybirsk)
- plasma sources
  - mcf – tokamak, stellarator (JET (dt)  $< 1 \cdot 10^{12} \text{ cm}^{-2} \text{ s}^{-1}$ , t < 10 s)
  - icf (NIF  $1 \cdot 10^9 \text{ cm}^{-2} \text{ imp}^{-1}$ )
  - z-pinch (NST DPF 1MJ (dt)  $\sim 1 \cdot 10^{11} \text{ cm}^{-2} \text{ imp}^{-1}$ )
- spallation source (ISIS  $3 \cdot 10^7 \text{ cm}^{-2} \text{ s}^{-1}$ )
- **MARIA LiD  $< 1 \cdot 10^{10} \text{ cm}^{-2} \text{ s}^{-1}$ , 4000 h/y, 60cm<sup>3</sup>**
- designed sources
  - ITER ( $4 \cdot 10^{14} \text{ cm}^{-2} \text{ s}^{-1}$ , t  $\approx 500$  s)
  - DEMO ( $1 \cdot 10^{15} \text{ cm}^{-2} \text{ s}^{-1}$ )
  - ESS ( $1 \cdot 10^{13} \text{ cm}^{-2} \text{ s}^{-1}$ )
  - IFMIF ( $\sim 8 \cdot 10^{14} \text{ cm}^{-2} \text{ s}^{-1}$ , 20 dpa/y, 500cm<sup>3</sup>)



## The neutron „conversion”



## The converters „history”

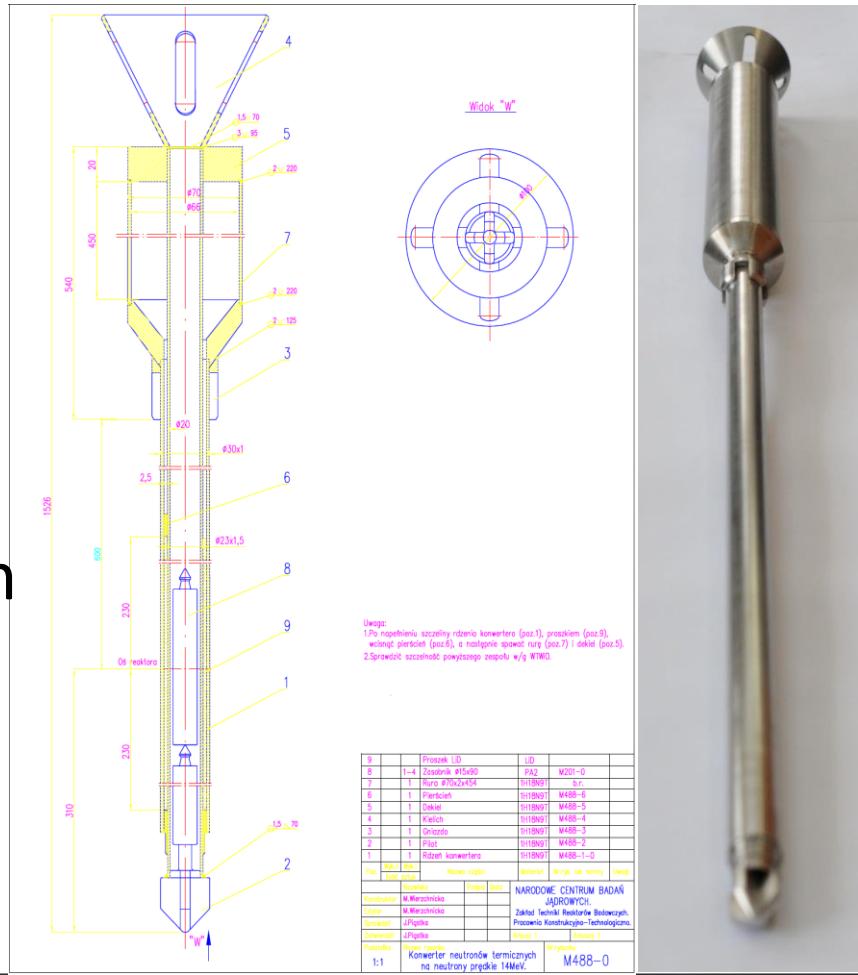
- TRIGA Mark II, Kansas –  ${}^6\text{LiOD}\cdot\text{D}_2\text{O}$ ,  $3\cdot10^4 \text{ cm}^{-2} \text{ s}^{-1}$ , 1976
- MURR, Missouri –  ${}^6\text{LiOD}\cdot\text{D}_2\text{O}$ ,  $32 \text{ cm}^3$ ,  $6\cdot10^4 \text{ cm}^{-2} \text{ s}^{-1}$ , 1982
- KUR, Kyoto –  ${}^6\text{LiD}$ ,  $100 \text{ cm}^3$ ,  $3\cdot10^5 \text{ cm}^{-2} \text{ s}^{-1}$ , 1988
- TRIGA Mark II, Wien –  ${}^6\text{LiD}$ ,  $4\cdot10^8 \text{ cm}^{-2} \text{ s}^{-1}$ , 1997
- IVV-2M, Zariechnyj –  $0.85\text{g } {}^6\text{LiD}$ ,  $1.3 \text{ cm}^3$ ,  $3\cdot10^{10} \text{ cm}^{-2} \text{ s}^{-1}$ , 2002
- MARIA, Świerk –  ${}^6\text{LiD}+{}^6\text{LiOD}\cdot\text{D}_2\text{O}$ ,  $60 \text{ cm}^3$ ,  $<1\cdot10^{10} \text{ cm}^{-2} \text{ s}^{-1}$ , 2014  
10 g      55 g

# The converter in MARIA reactor

- converting materials
- conversion efficiency
- geometry optimization
- neutronic calculations
- thermo-hydraulic calculations
- reactivity calculations
- safety analysis
- converter design
- converter construction
- operation procedures
- regulator permission

# Converter construction

- cylindrical shape
- concentric vertical tubes
- cylindrical converting layer (2.5 mm thick, 35 cm high) surrounds container Ø18mm
- flowing down water cooling inner and outer clad
- gas expansion chamber 1.4 l

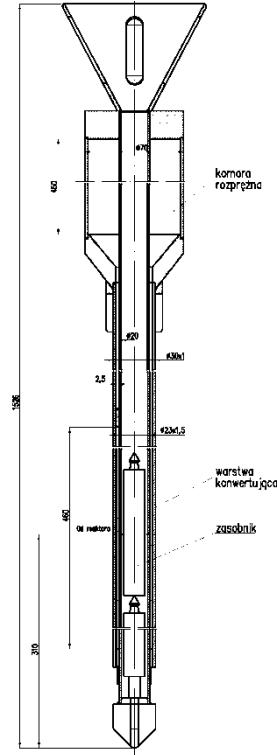


# Converting materials

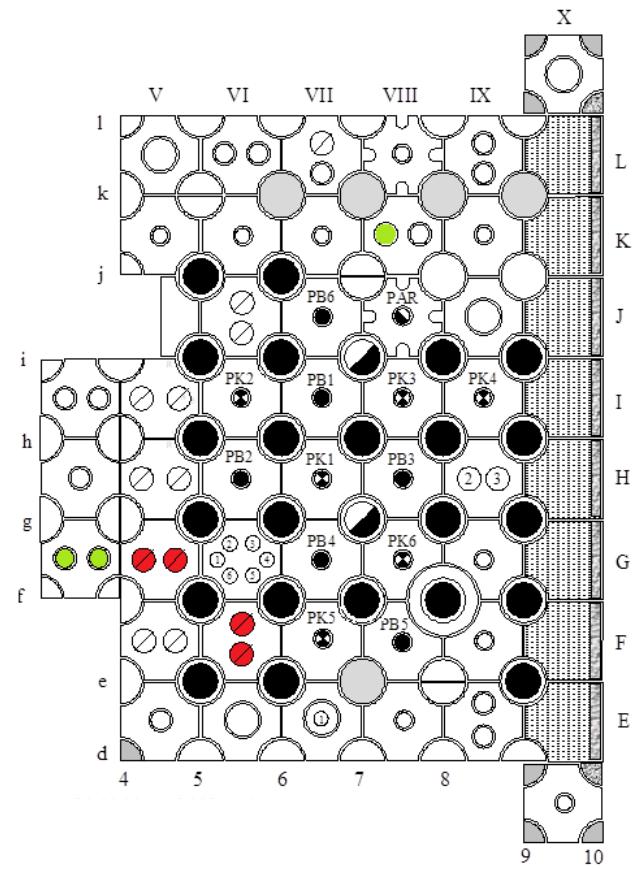
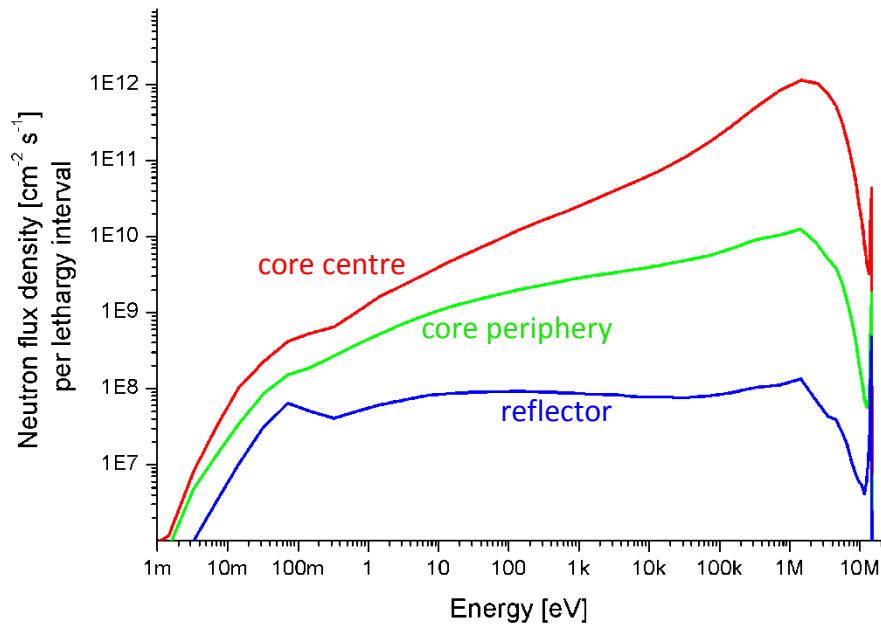
- ${}^6\text{LiD}$  (10 g),  ${}^6\text{LiOD}\cdot\text{D}_2\text{O}$  (55 g)
- conversion efficiency

Converting material	Reaction probability	
	T - D	T - ${}^6\text{Li}$
${}^6\text{LiD}$	$1.71\cdot 10^{-4}$	$0.84\cdot 10^{-4}$
${}^6\text{LiOD}\cdot\text{D}_2\text{O}$	$1.28\cdot 10^{-4}$	$0.19\cdot 10^{-4}$

- thermal neutron flux density  $0.5\cdot 10^{14} \text{ cm}^{-2} \text{ s}^{-1}$
- 14 MeV neutron flux density  $0.5\cdot 10^{10} \text{ cm}^{-2} \text{ s}^{-1}$

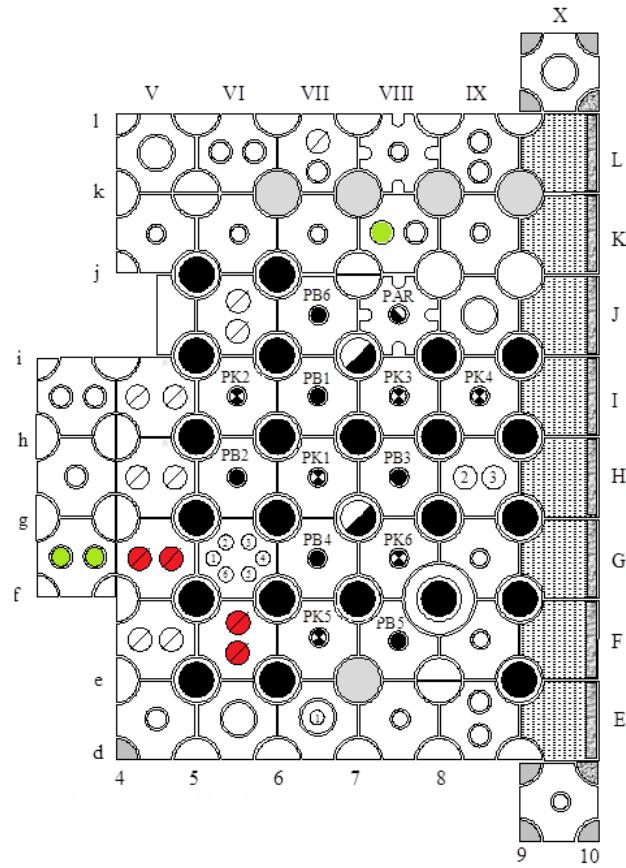


# Neutronic calculations



# Reactivity perturbation

Location	Reactivity [\\$]
J-IX/A	- 0.15
J-IX/B	- 0.20
G-IV/A	- 0.10
G-IV/B	- 0.19
G-V/A	- 0.49
G-V/B	- 0.77
K-VIII/A	- 0.06



## Operation conditions

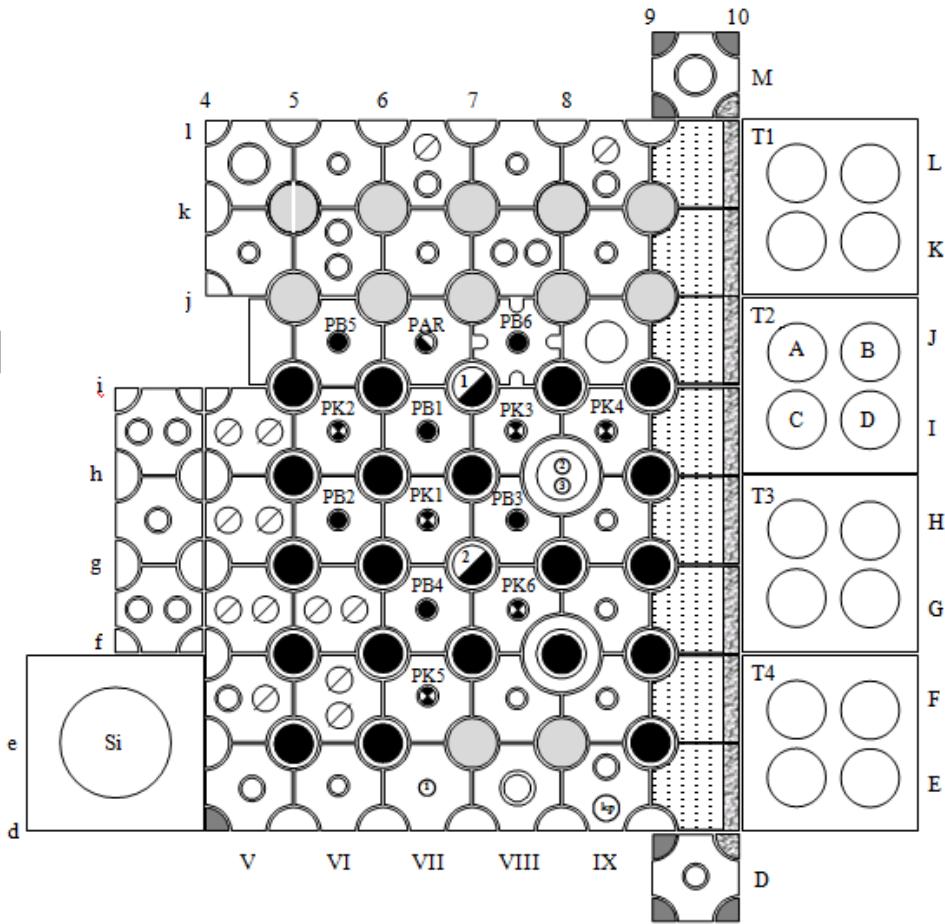
- heat generation
  - cooling water heating 40°C
  - max clad temperature 100°C
  - max temp. of converting layer 320°C
- after 2800 h operation (neutron fluence  $5 \cdot 10^{20} \text{cm}^{-2}$ )
  - tritium activity 280 TBq
  - gas pressure inside converter – 1.0 MPa

## Testing operation

- 18/09/2014 ÷ 24/09/2014, 134.5 h
- channel K-VIII/A (reactivity -0.06\$)
- max clad temperature 80°C
- irradiated targets: steel samples, activation detectors
- thermal neutron flux density  $0.5 \cdot 10^{14} \text{ cm}^{-2} \text{ s}^{-1}$
- 14 MeV neutron flux density  $\sim 0.5 \cdot 10^{10} \text{ cm}^{-2} \text{ s}^{-1}$

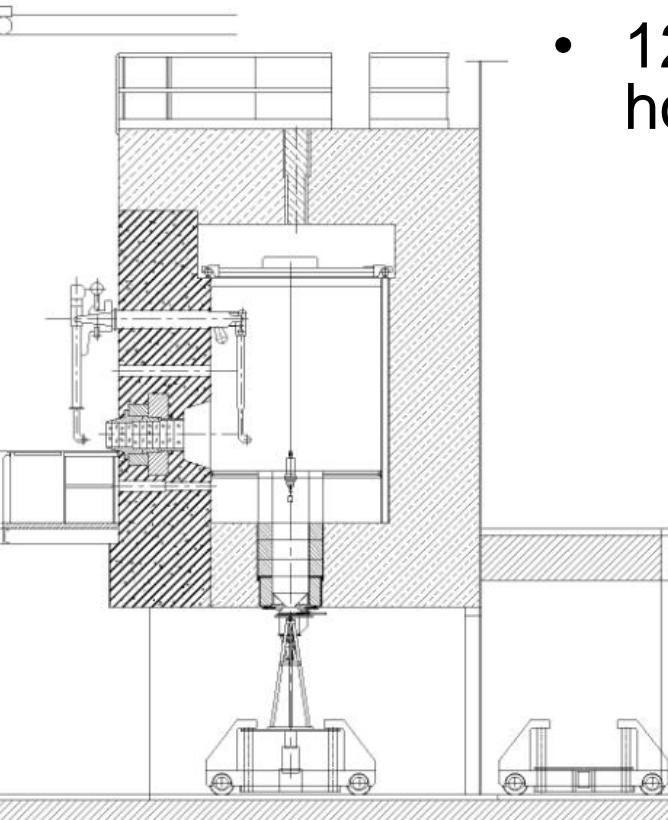
# Fast neutron irradiation channels

- fast neutron (Watt spc.) flux density up to  $3 \cdot 10^{12} \text{ cm}^{-2} \text{ s}^{-1}$
- thermal neutron flux reduced down to  $3 \cdot 10^{10} \text{ cm}^{-2} \text{ s}^{-1}$
- 16 irradiation channels ( $\varnothing 90 \text{ mm} \times 900 \text{ mm}$ )
- possible irradiation of samples, apparatus, etc.



# Post-irradiation examination

- 3 reactor hot cells ( $10^{12}\div 10^{15}$  Bq) with instrumentation
  - 12 NCBJ Material Research Laboratory hot cells ( $10^{12}$  Bq) with instrumentation
    - transport system of radioactive materials from reactor



## Future prospects

- fast neutron irradiation inside purpose-build fuel element
  - fast neutron (Watt spc.) flux density over  $2 \cdot 10^{14} \text{ cm}^{-2} \text{ s}^{-1}$
  - thermal neutron flux density up to  $3 \cdot 10^{14} \text{ cm}^{-2} \text{ s}^{-1}$
  - channel  $\sim \varnothing 15 \div 45 \text{ mm}$
- out-of-reactor (on horizontal channel)  
thermal to 14 MeV neutron converter
  - 14 MeV neutron flux density  $\sim 1 \cdot 10^6 \text{ cm}^{-2} \text{ s}^{-1}$ , no gamma ray
  - irradiation of large size apparatus, devices, etc.,
  - operation 4000 h/year